

DESCRIPTION

SiC-HEXAGONAL FERRITE TYPE CERAMIC COMPOSITE ELECTROMAGNETIC
WAVE ABSORBER

5

Technical Field

The present invention relates to an electromagnetic
wave absorber which is composed of a composite sintered
product of a hexagonal ferrite and SiC, and which exhibits
.10 high absorption over a wide band in a high-frequency band
(GHz band).

Background Art

In recent years, frequencies used for wireless LANs,
15 intelligent transport systems (ITS), next-generation
cellular phones, and the like have been changed from a MHz
band to a GHz band in which high-speed and high-volume
information transmission can be conducted.

In this band, carbon-containing resins and the like are
20 primarily used for electromagnetic wave absorbers to prevent
malfunctions of equipment at present. However, the width of
the absorption band is narrow, and there are heat resistance
and other problems.

A spinel ferrite is also used for an electromagnetic
25 wave absorber. However, it is difficult to use this in the

GHz band because of a snake phenomenon (natural resonance occurs in the neighborhood of 1 GHz and, thereby, no absorption is effected in a high-frequency region higher than that).

5 The inventors of the present invention previously found that a composite sintered product of a spinel ferrite and SiC is effective as an electromagnetic wave absorber in the GHz band (the absorption in the GHz band is based on SiC), and filed an application for a patent (Non-Patent Document 1
10 and Patent Document 1).

 This composite sintered product is produced by combining a spinel ferrite (absorption frequency is a few hundred megahertz) that is a magnetic loss material and SiC (absorption frequency is 10 GHz or more) that is a
15 dielectric loss material. However, only the magnetic loss is manifested, and there is a problem in that although the absorption frequency is increased up to the GHz band, the absorption width is narrow.

 It is also known that the hexagonal ferrite serves as
20 an electromagnetic wave absorber in the GHz band (Non-Patent Documents 2 to 4). The resonant frequency of M-type $\text{BaFe}_{12}\text{O}_{19}$ is 50 GHz. The resonant frequency of $\text{Ba}[\text{Fe}_{12-x}(\text{Ti}_{0.5}\text{Mn}_{0.5})_x]\text{O}_{19}$ in which Ti and Mn have substituted for Fe is 16 GHz where the amount of substitution $x = 2.5$, and the
25 resonant frequency is 6 GHz where $x = 4.5$. The resonant

frequency of Ferroxplana-type $\text{Ba}_2\text{Co}_2\text{Fe}_{12}\text{O}_{22}$ (Y type) is 5 to 10 GHz, and the resonant frequency of $\text{Ba}_3\text{Co}_2\text{Fe}_{24}\text{O}_{41}$ (Z type) is 1 GHz. There are also problems in that, for example, the width of the absorption band is small.

5 Non-Patent Document 1 J. Takada et al.,

"Pureseramikkusuhou niyoru feraitokei hukugouzairyono sakuseito denpakyusyutokusei (Preparation of ferrite composite material by pre-ceramics method and wave absorption characteristics)", J. Magn. Soc. Jpn., Vol. 26,

10 No. 6, p818-822 (2002)

Non-Patent Document 2 M. Hanazawa et al., "M-gata roppousyo feraitoo mochiita 40 GHz taiyo denpakyusyutaino koutaiikikani kansuru kentou (Study on band-widening of 40-GHz-band wave absorber including M-type hexagonal ferrite)",

15 Denshijouhou tsuushingakkai taikaikouen ronbunshu

(Proceedings of IEICE Conference), Vol. 2002, Tsuushin (Communication) 1 PAGE, 384 (2002)

Non-Patent Document 3 T. Inui et al., "Roppousyo Mg_2Y feraitoo mochiita koutaiiki denpakyusyutai (Wide-band wave absorber including hexagonal Mg_2Y ferrite)", Denshijouhou

20 tsuushingakkai taikaikouen ronbunshu (Proceedings of IEICE Conference), Vol. 1999, Sougou (General) 2 PAGE, 340 (1999)

Non-Patent Document 4 H. Ota et al., "M-gata roppousyo feraito hukugoutai shitono hokusotoujiritsuto

25 denpakyusyutokusei (Complex magnetic permeability and wave

absorption characteristics of M-type hexagonal ferrite composite sheet)", Denshijouhou tsuushingakkai taikaikouen ronbunshu (Proceedings of IEICE Conference), Vol. 2000, Sougou (General) 2 PAGE, 728-729 (2000)

5 Patent Document 1 Japanese Unexamined Patent Application Publication No. 2002-37662

Disclosure of Invention

The inventors of the present invention found that an
.10 electromagnetic wave absorber exhibiting a high amount of absorption over a wide frequency range in the GHz band was able to be provided by composite-sintering a hexagonal ferrite and electrically conductive SiC.

That is, the present invention relates to (1) a SiC-
15 hexagonal ferrite type ceramic composite electromagnetic wave absorber for a high-frequency band, the electromagnetic wave absorber characterized by being composed of a composite sintered product of a hexagonal ferrite and SiC.

The present invention relates to (2) the
20 electromagnetic wave absorber according to the above-described item (1), characterized in that SiC is produced by incorporating 1 to 5 percent by weight of SiC powder or fiber into the hexagonal ferrite.

The present invention relates to (3) the
25 electromagnetic wave absorber according to the above-

described item (1), characterized in that SiC is produced by incorporating 1 to 5 percent by weight of curing-treated SiC precursor into the hexagonal ferrite.

The present invention relates to (4) the
5 electromagnetic wave absorber according to any one of the above-described items (1) to (3), characterized in that the hexagonal ferrite is of Y-type or Z-type.

The present invention relates to (5) the
electromagnetic wave absorber according to any one of the
10 above-described items (1) to (3), characterized in that the hexagonal ferrite is $\text{Ba}_2\text{Ni}_2\text{Fe}_{12}\text{O}_{22}$ or $\text{Ba}_3\text{Co}_2\text{Fe}_{24}\text{O}_{41}$.

The present invention relates to (6) a method for producing the electromagnetic wave absorber according to the above-described item (2), the method characterized by
15 including the steps of incorporating 1 to 5 percent by weight of SiC powder or fiber into a hexagonal ferrite together with a sintering additive, followed by molding, and conducting sintering at 700°C to 900°C.

The present invention relates to (6) a method for
20 producing the electromagnetic wave absorber according to the above-described item (3), the method characterized by including the steps of incorporating 1 to 5 percent by weight of curing-treated SiC precursor into a hexagonal ferrite, followed by molding, and conducting sintering.

25 The ferrite is a generic name for magnetic oxides

containing Fe_2O_3 as a primary component, and a) a spinel ferrite, b) a hexagonal ferrite, c) garnet type, and d) perovskite type are included. The hexagonal ferrite is an iron oxide based magnetic material containing Ba and the like. The crystal structure is hexagonal, and ① Magnetoplumbite (M) type and ② Ferroplana type (Y type, X type, Z type, W type, and U type) are included. Typical Ferroplana type is the Y type or the Z type.

The composition of the hexagonal ferrite is shown by, for example, an equilibrium diagram of $\text{BaO-AO-Fe}_2\text{O}_3$. Here, Sr, Pb, or the like may substitute for Ba in BaO. A divalent metal, Mg, Co, Ni, Cu, Zn, or the like is represented by A.

The electrically conductive SiC takes an action to absorb an electromagnetic wave only after the SiC is dispersed into an insulating material, e.g., a hexagonal ferrite. The absorption wavelength of SiC varies depending on the production history of SiC. The absorption wavelength is about 8 GHz when SiC originates from an inorganic polymer, polycarbosilane (PCS), and is about 10 GHz when a SiC powder is incorporated.

As described above, the ferrite exhibits electromagnetic wave absorption based on the magnetic loss, and SiC exhibits electromagnetic wave absorption based on the dielectric loss. The inventors of the present invention

combined the two, and succeeded in realization of an electromagnetic wave-absorbing composite sintered product having a wide absorption width and a high amount of absorption in the GHz band while taking advantage of the magnetic loss and the dielectric loss in combination. Fig. 1 shows the concept of band-widening taking advantage of the magnetic loss and the dielectric loss in combination.

For example, $\text{Ba}_2\text{Ni}_2\text{Fe}_{12}\text{O}_{22}$ (denoted as Ni_2Y in the present specification) or $\text{Ba}_3\text{Co}_2\text{Fe}_{24}\text{O}_{41}$ (denoted as Co_2Z in the present specification) is used as the hexagonal ferrite. The electromagnetic wave absorption region can be variously changed in the GHz region by selecting the composition of the hexagonal ferrite and SiC. For example, a composite in which a few percent by weight of SiC has been incorporated into a Y-type hexagonal ferrite exhibits electromagnetic wave absorption double peaks at 7 GHz and 11 GHz (the former is based on the hexagonal ferrite magnetic loss, and the latter is based on the SiC dielectric loss). The absorption width at the amount of absorption of -15 dB is 6 GHz and, therefore, the composite has a wide absorption width and a high amount of absorption.

This composite sintered product can be produced by ① incorporating a small amount of SiC powder or fiber into the hexagonal ferrite and conducting low-temperature sintering together with a sintering additive (a low-temperature

sintering method), or ② incorporating a small amount of curing-treated SiC precursor into the hexagonal ferrite and conducting sintering (a pre-ceramics method). The low-temperature sintering method of item ① is a preferable
5 production method since it can be applied to every hexagonal ferrite. The pre-ceramics method of item ② can be applied to limited hexagonal ferrites.

Brief Description of the Drawings

10 Fig. 1 is a conceptual diagram showing that band-widening is intended by combining different materials to take advantage of the magnetic loss and the dielectric loss in combination. Fig. 2 is a flow chart of a low-temperature sintering method to produce the electromagnetic wave
15 absorber of the present invention. Fig. 3 is a flow chart of a pre-ceramics method to produce the electromagnetic wave absorber of the present invention. Fig. 4 is a graph showing the electromagnetic wave absorption characteristics of sintered products produced in Example 1. Fig. 5 is a
20 graph showing the electromagnetic wave absorption characteristics of sintered products produced in Example 2. Fig. 6 shows graphs of the measurement results of the complex magnetic permeability and the complex dielectric constant of the sintered product produced in Example 2.

25

Best Mode for Carrying Out the Invention

① Low-temperature sintering method

Fig. 2 shows a flow chart of a typical low-temperature sintering method.

5 A high-temperature heat treatment is required to produce a sintered composite of a hexagonal ferrite, e.g., Ni_2Y , and SiC . As the temperature is increased, Ba reacts with Si, and the composition is shifted, so that the characteristics of the ferrite are deteriorated. Therefore, a sintering additive is used and low-temperature sintering is conducted. Preferably, the sintering additive is B_2O_3 . However, other sintering auxiliaries may be used as long as they are metal oxides, e.g., Bi_2O_3 , PbO , and V_2O_5 , and they can facilitate composite-sintering of the hexagonal ferrite and SiC . The additive is specified to be 0.2 to 10 percent by weight, and preferably be 1 to 5 percent by weight. The sintering temperature depends on types of the hexagonal ferrite and the sintering additive. If the sintering temperature is increased to $1,200^\circ\text{C}$, breakdown of the ferrite, reaction with the additive, and the like occur and, therefore, this is not preferable. The sintering temperature is preferably 700°C to 900°C in the air.

② Pre-ceramics method

Fig. 3 shows a flow chart of a typical pre-ceramics method.

Polycarbosilane (PCS), which is a silicon based ceramic-forming precursor $(-\text{SiHCH}_3-\text{CH}_2-)_n$, is curing-treated. The curing treatment is a treatment to form a SiO_2 film on the surface of a PCS powder, and the treatment method itself is a publicly known means (refer to the above-described Patent Document 1). That is, the curing treatment includes a thermal oxidation curing method in which a PCS surface is oxidized by a heat treatment conducted at a temperature range of about 200°C to 600°C in an oxidizing atmosphere, for example, in the air, for about 10 hours or more so as to form a SiO_2 oxide film and an electron beam curing method in which Si-Si bonds are formed by applying an electron beam or a γ ray to the PCS surface so as to form a film.

Preferably, the mixing ratio of PCS to Ba hexagonal ferrite is 1 to 30 percent by weight, and more preferably is 2 to 10 percent by weight. A primary heat treatment is conducted at 900°C to $1,200^\circ\text{C}$ in an inert gas, and a secondary heat treatment is conducted at 900°C to $1,200^\circ\text{C}$, preferably in the neighborhood of $1,000^\circ\text{C}$, in the air.

(EXAMPLES)

EXAMPLE 1

A Ba ferrite (Co_2Z : Z type) powder was prepared as a raw material by mixing BaCO_3 , CoO , and Fe_2O_3 at a ratio of $\text{Ba}:\text{Co}:\text{Fe} = 3:2:24$ and conducting sintering at $1,200^\circ\text{C}$ for 6 hours. The resulting BaCo_2Z powder was mixed with 1 percent

by weight of B_2O_3 (Sigma-Aldrich Japan K.K. SAJ analytical reagent grade: purity 90%) and 5 percent by weight of SiC fiber (SiC fiber produced by Nippon Carbon Co., Ltd.). The resulting mixed powder was press-molded into the shape of a pellet to prepare three samples, followed by sintering in the air at $700^\circ C$ for 6 hours. The thicknesses of the three samples were 2.6 mm, 3.1 mm, and 4.0 mm, respectively. In addition, a sample of 3.7 mm in thickness was prepared as a comparative example by sintering a Co_2Z powder alone.

A composite sintered product of Co_2Z and the SiC fiber was produced through low-temperature sintering by using B_2O_3 as a sintering additive. The resulting sintered product was subjected to a powder X-ray diffraction measurement, texture observation with a scanning electron microscope (SEM), and a measurement of the amount of wave absorption with a network analyzer. Fig. 4 shows each of the electromagnetic wave absorption characteristics of the four samples. It was made clear that the sample of 3.1 mm in thickness had the dielectric loss and the magnetic loss in combination and exhibited absorption over a wide frequency range. Although the amount of absorption did not reach -20 dB of complete absorption, an absorption width of 6.8 GHz was exhibited at -10 dB.

EXAMPLE 2

A Ba ferrite (Ni_2Y : Y type) powder was prepared as a raw

material by mixing BaCO_3 , NiO , and Fe_2O_3 at a ratio of
Ba:Ni:Fe = 2:2:12 and conducting sintering in the air at
1,200°C for 6 hours. The resulting Ni_2Y powder was mixed
with 3 percent by weight of curing-treated PCS. The curing
5 treatment was conducted in the air at 500°C for 10 hours.
The resulting mixed powder was press-molded into the shape
of a pellet to prepare three samples, followed by primary
sintering in an Ar atmosphere at 1,000°C for 6 hours.
Thereafter, three samples were subjected to secondary
10 sintering in the air at 1,000°C (a), 1,100°C (b), and
1,200°C (c), respectively, for 6 hours.

The resulting sintered products of three samples were
subjected to the powder X-ray diffraction measurement, the
texture observation with the scanning electron microscope
15 (SEM), and the measurement of the amount of wave absorption
with the network analyzer as in Example 1. Fig. 5 shows
each of the electromagnetic wave absorption characteristics
of (a), (b), and (c). The absorption characteristics became
deteriorated as the secondary sintering temperature was
20 increased. However, although the sample which had been
subjected to the secondary sintering at 1,000°C did not
reach -20 dB of complete absorption, an absorption width of
6.2 GHz was exhibited at -15 dB. It is clear from this that
a preferable secondary sintering temperature is 1,000°C or
25 less.

Fig. 6 shows the measurement results of the complex magnetic permeability (μ_r) and the complex dielectric constant (ϵ_r) of the sample which had been subjected to the secondary sintering at 1,000°C. It is clear from this that
5 a composite sintered product having the magnetic loss and the dielectric loss in combination was produced.

Industrial Applicability

In the advanced information and communications society
10 expected to rapidly progress and develop in the future, electromagnetic wave absorbers in the GHz band become indispensable. Therefore, there is a high possibility of commercialization of the high-performance electromagnetic wave absorber for the GHz band according to the present
15 invention.